

Nonsmooth Differential- Algebraic Equations

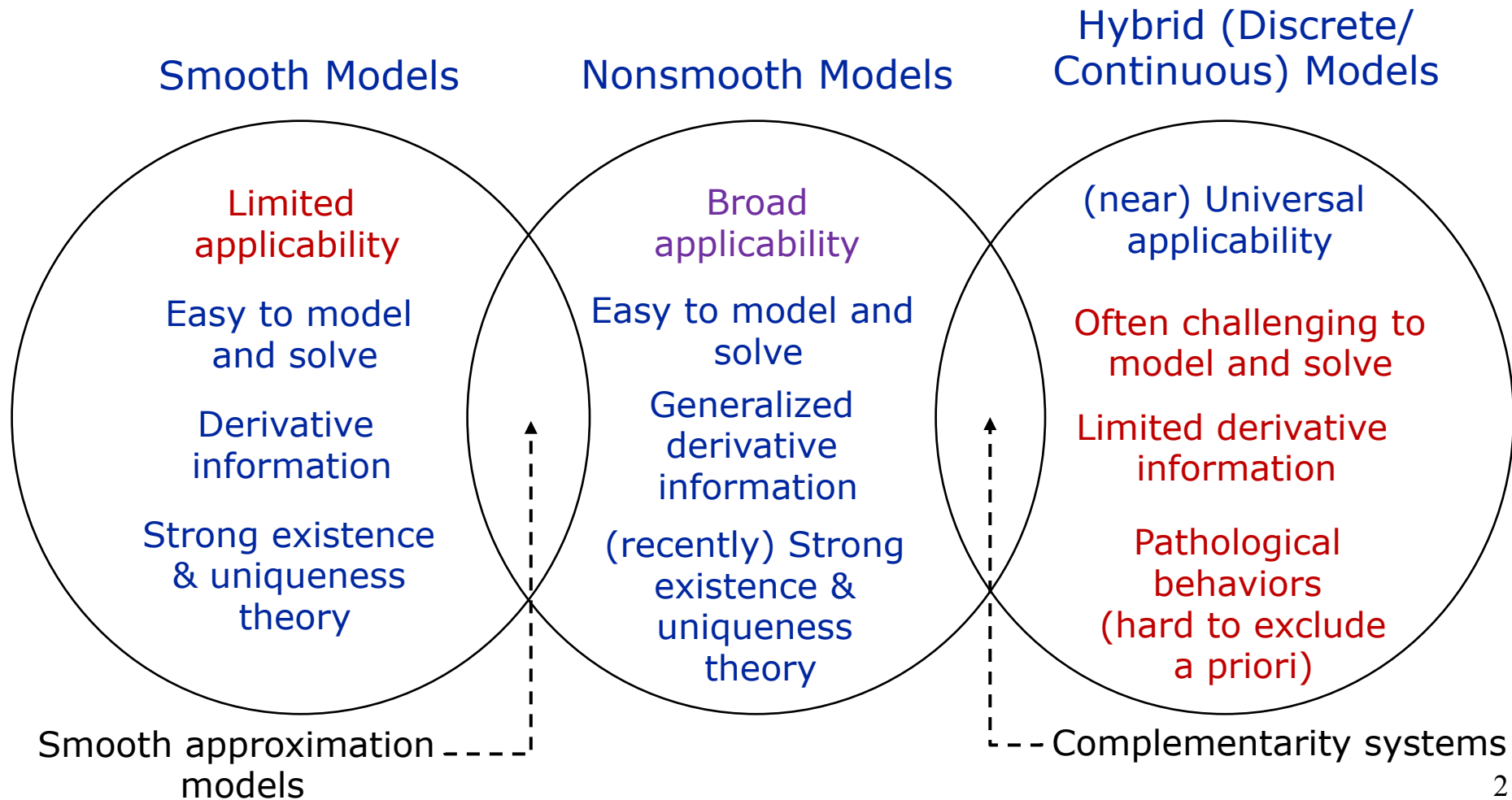
Paul I. Barton

*Process Systems Engineering Laboratory
Massachusetts Institute of Technology*



Dynamic Modeling Frameworks in PSE

- ◆ Trade-off: applicability vs. ease of modeling & solving



Hybrid Automaton Framework

- ◆ Simple const. P flash process:

$$\dot{H}(t) = U(T_{out} - T(t))$$

$$M = M_L(t) + M_V(t)$$

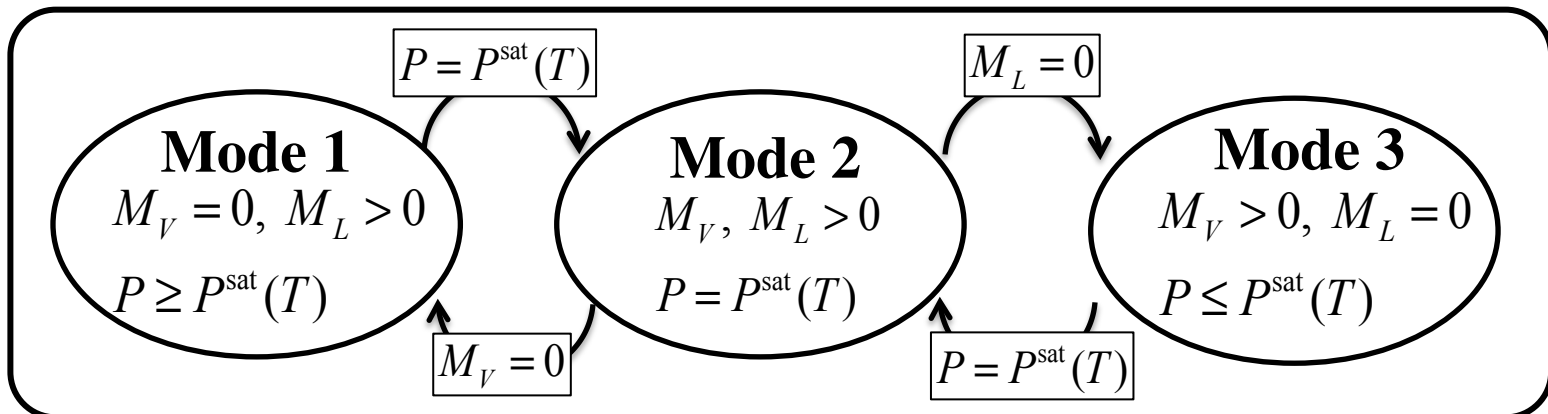
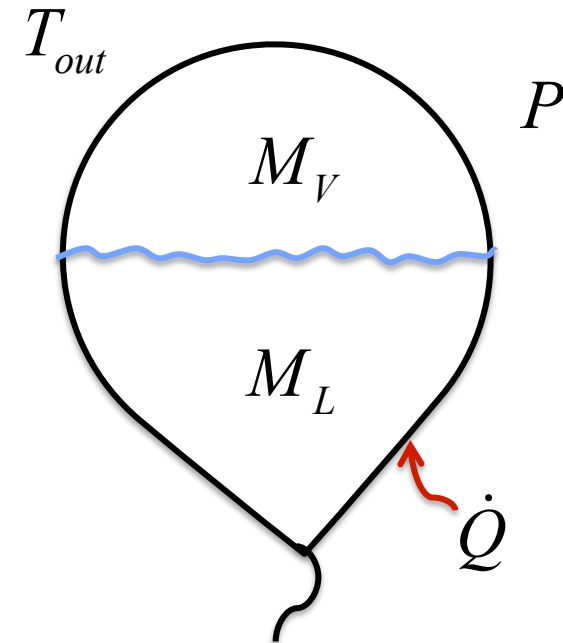
$$H(t) = Mh_V(t) - M_L(t)\Delta h_{vap}(T(t))$$

$$h_V(t) = Cp(T(t) - T_0)$$

$$\log(P^{sat}(t)) = A - B/(T(t) + C)$$

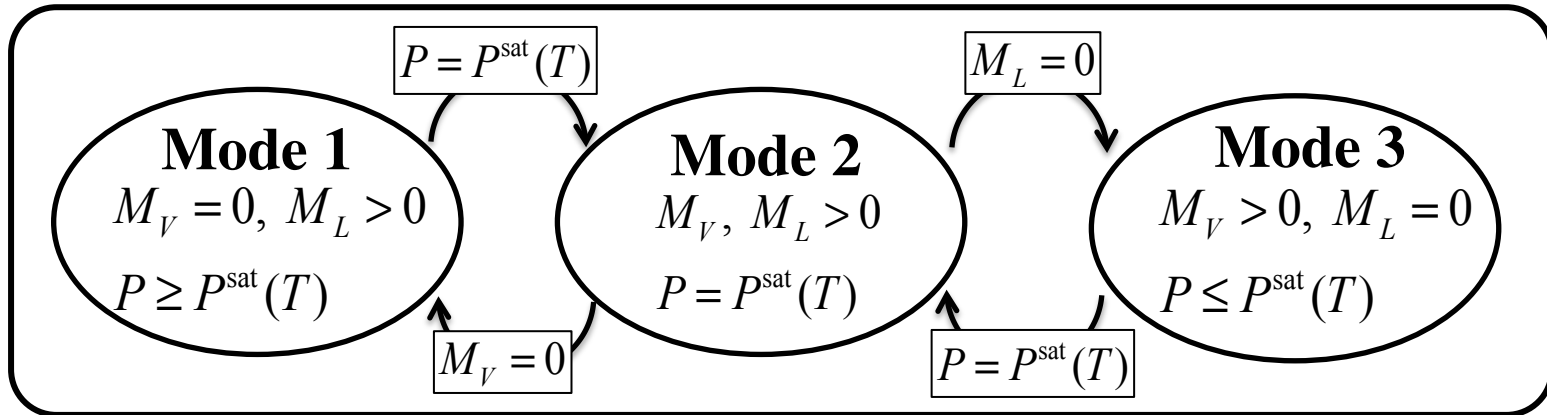
⋮

- DAE embedded in hybrid automaton



Hybrid vs. Nonsmooth

◆ Hybrid automaton formulation



◆ “Continuous” disjunction:

$$\begin{bmatrix} M_V(t) = 0 \\ M_L(t) > 0 \\ P \geq P^{\text{sat}}(T(t)) \end{bmatrix} \otimes \begin{bmatrix} M_V(t) > 0 \\ M_L(t) > 0 \\ P = P^{\text{sat}}(T(t)) \end{bmatrix} \otimes \begin{bmatrix} M_V(t) > 0 \\ M_L(t) = 0 \\ P \leq P^{\text{sat}}(T(t)) \end{bmatrix}$$

Hybrid vs. Nonsmooth

- ◆ “Continuous” disjunction:

$$\begin{bmatrix} M_V(t) = 0 \\ M_L(t) > 0 \\ P \geq P^{\text{sat}}(T(t)) \end{bmatrix} \otimes \begin{bmatrix} M_V(t) > 0 \\ M_L(t) > 0 \\ P = P^{\text{sat}}(T(t)) \end{bmatrix} \otimes \begin{bmatrix} M_V(t) > 0 \\ M_L(t) = 0 \\ P \leq P^{\text{sat}}(T(t)) \end{bmatrix}$$

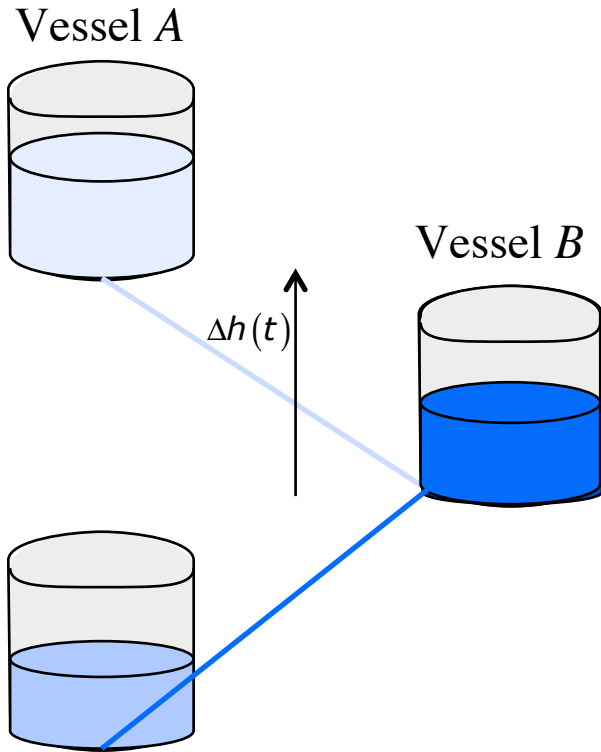
- ◆ Nonsmooth equation:

$$0 = \text{mid} \left(M_V(t), P - P^{\text{sat}}(T(t)), -M_L(t) \right)$$

Nonsmooth Models: Applications

- ◆ Intensive properties with flow reversals
- ◆ Flow transitions (laminar, turbulent, choked)
- ◆ Thermodynamic phase changes
- ◆ Crystallization kinetics: growth vs. dissolution
- ◆ Flow control devices, diodes
- ◆ Irregularities in vessel geometry
- ◆ Dynamic flux balance analysis (DFBA) systems
 - e.g., aerobic to anaerobic switch
- ◆ Various “elements” of controllers
- ◆ Protecting domains of functions (abs)
- ◆ Piecewise properties
- ◆ etc., etc.

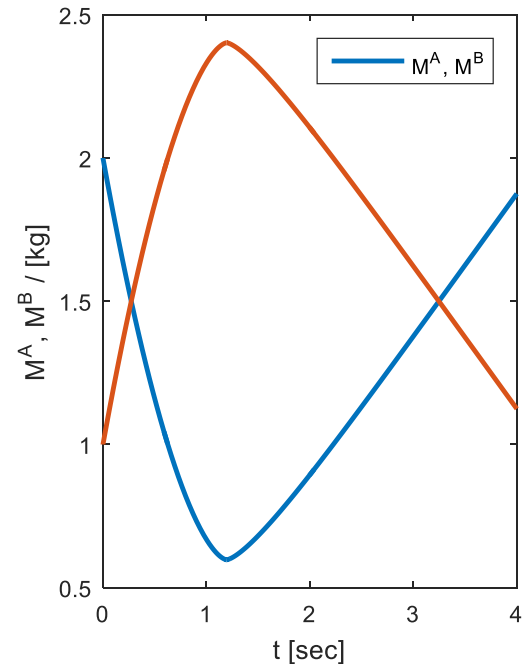
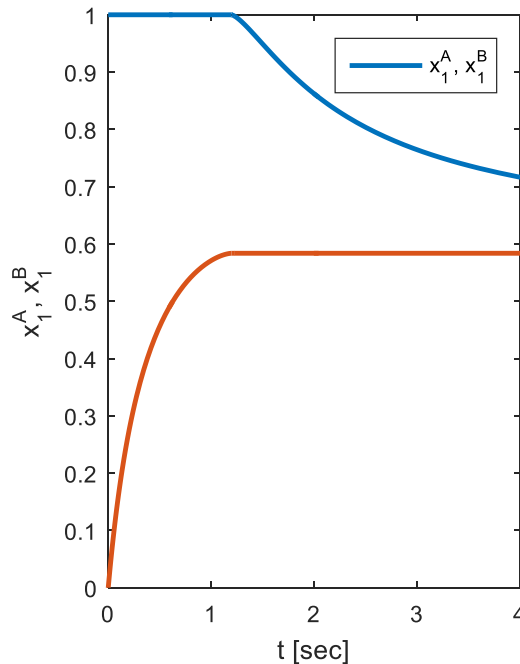
Flow Reversal: Intensive Properties



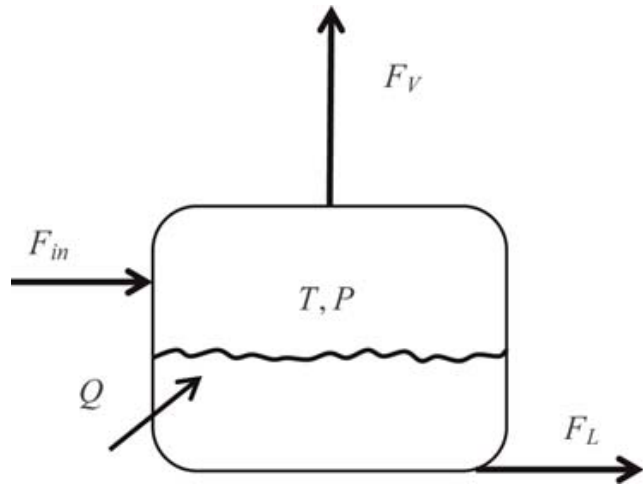
$$\frac{dM_i^A}{dt}(t) = -\left(\max(F_{out}^A(t), 0)x_i^A + \min(F_{in}^B(t), 0)x_i^B\right)$$

$$\frac{dM_i^B}{dt}(t) = -\frac{dM_i^A}{dt}(t); \quad F_{out}^A(t) = F_{in}^B(t)$$

$$F_{out}^A(t) = c \frac{h^A(t) - h^B(t) + \Delta h(t)}{\sqrt{|h^A(t) - h^A(t) + \Delta h(t)|} + \varepsilon}$$



Multi-component Dynamic VLE



Thermodynamic phase equilibrium:

$$y_i(t) = k_i(t)x_i(t)$$

$$0 = \text{mid} \left(\frac{M_V(t)}{M_V(t) + M_L(t)}, \sum_{i=1}^{n_c} x_i(t) - \sum_{i=1}^{n_c} y_i(t), \frac{M_V(t)}{M_V(t) + M_L(t)} - 1 \right)$$

Mass and energy balances:

$$\frac{dM_i}{dt}(t) = F_{in}(t)z_i(t) - F_L(t)x_i(t) - F_V(t)y_i(t)$$

$$\frac{dU}{dt}(t) = F_{in}(t)h_{in}(t) - F_L(t)h_L(t) - F_V(t)h_V(t) + Q(t)$$

$$M_i(t) = M_L(t)x_i(t) + M_V(t)y_i(t)$$

$$\sum_{i=1}^{n_c} M_i(t) = M_L(t) + M_V(t)$$

$$H(t) = M_L(t)h_L(t) + M_V(t)h_V(t)$$

$$H(t) = U(t) + P(t)V$$

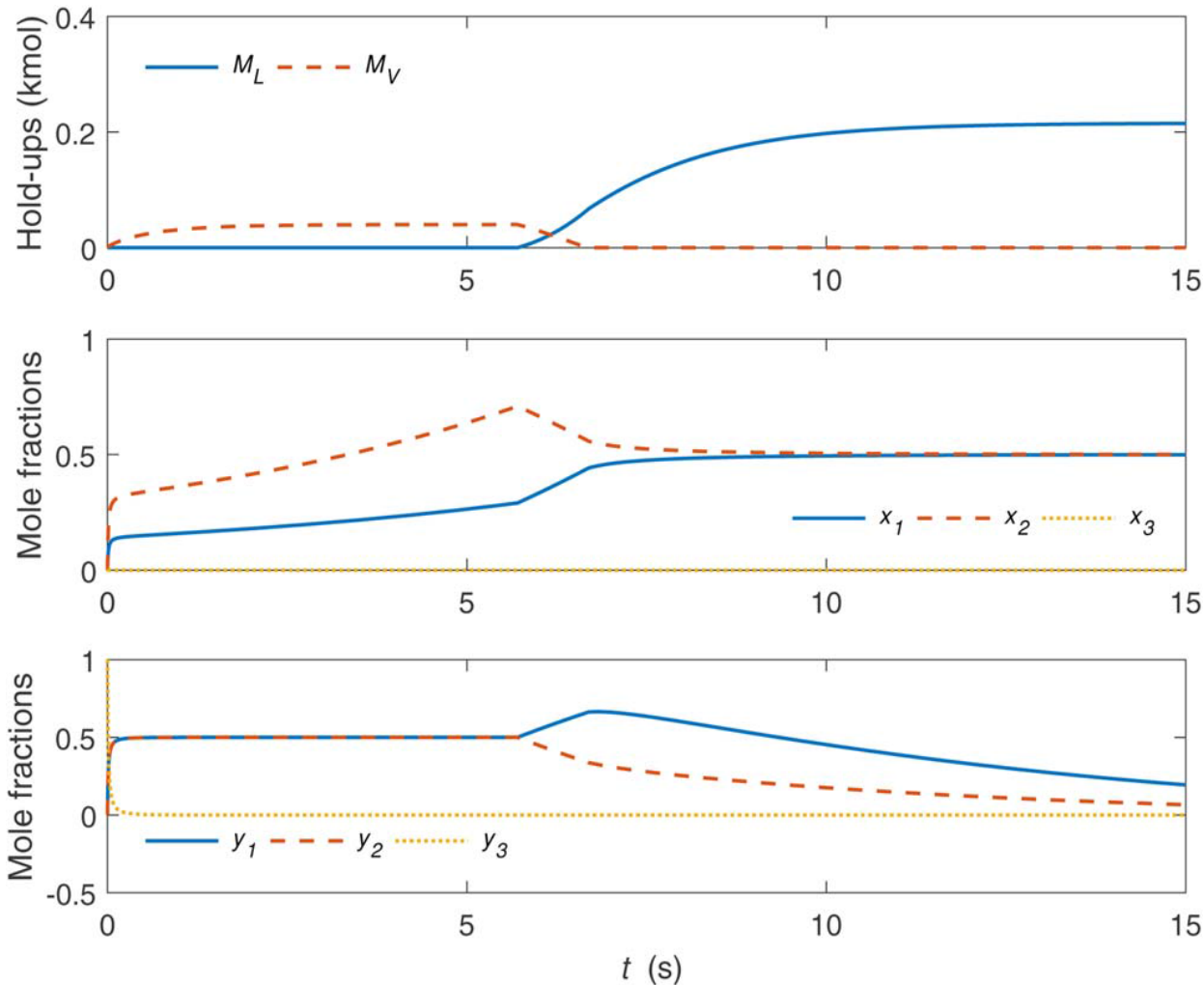
Flow control:

$$F_V(t) = c_v \min(V_V^{\min}, V_V(t)) \max \left(0, \frac{P(t) - P_0}{\sqrt{|P(t) - P_0|} + \varepsilon} \right)$$

$$F_L(t) = c_l \min(V_L^{\min}, V_L(t)) \max \left(0, \frac{K_L(t)}{\sqrt{|K_L(t)|} + \varepsilon} \right)$$

$$K_L(t) = g \frac{V_L(t)}{A} + \frac{P(t) - P_0}{\rho_L(t)}$$

Multi-component Phase Change



$$M_L = 0$$

$$\sum_{i=1}^{n_c} x_i(t) \leq 1$$

$$M_V = 0$$

$$\sum_{i=1}^{n_c} y_i(t) \leq 1$$

Crystallization Kinetics

- ◆ With the development of continuous crystallization processes, dissolution has to be considered in dynamic models of crystal size distribution:

$$\frac{\partial(Vn)}{\partial t}(t, z) + K(t) \frac{\partial(Vn)}{\partial z}(t, z) = Q_{in}(t)n_{in}(t, z) - Q_{out}(t)n(t, z)$$

$$S(t) = (x_i(t) - x_i^{sat}) / x_i^{sat}, \quad K(t) = \min\left(k_D S(t) |S(t)|^{n_D-1}, k_G |S(t)|^{n_G}\right)$$

- ◆ With finite volume discretization of the size coordinate:

$$\frac{dN_j}{dt}(t) + \frac{1}{\Delta z} \left(G(t) (N_j(t) - N_{j-1}(t)) + D(t) (N_{j+1}(t) - N_j(t)) \right) = Q_{in}(t)n_{j,in}(t) - Q_{out}(t)n_j(t), \quad j = 2, \dots, m-1$$

$$G(t) = \max\left(0, k_G S(t) |S(t)|^{n_G-1}\right)$$

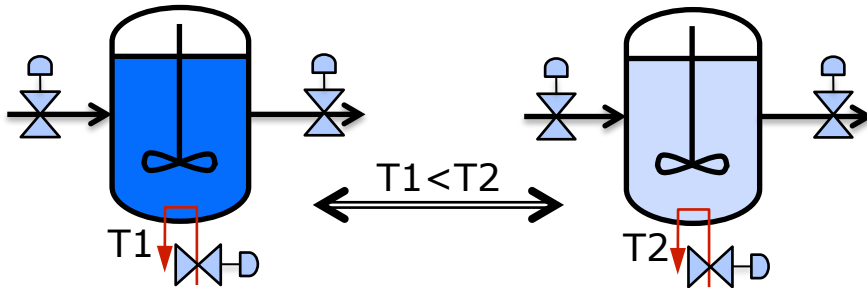
$$D(t) = \min\left(k_D S(t) |S(t)|^{n_D-1}, 0\right)$$

$$N_j \equiv Vn_j,$$

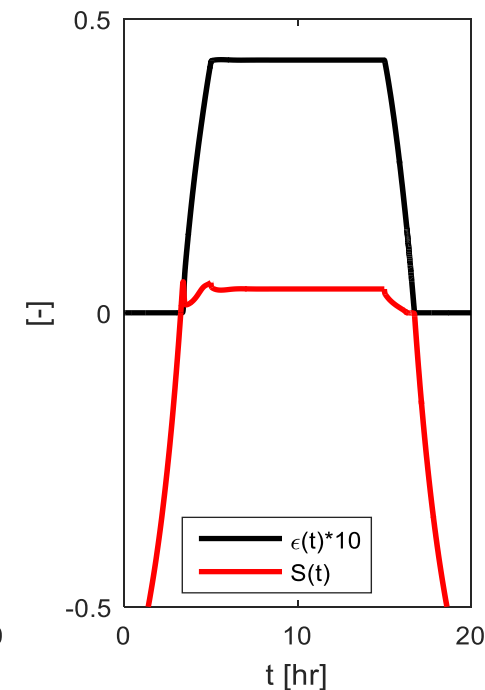
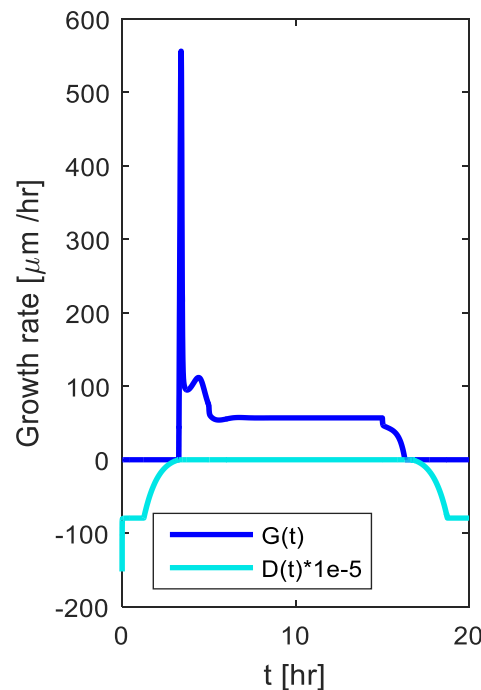
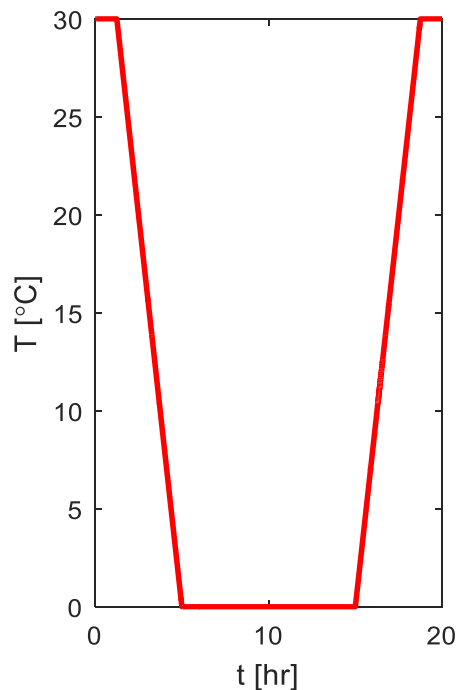
n_j – density of crystals of size $(j-1)\Delta L < L < j\Delta L$

Crystallization Kinetics

- Switching between regimes of positive and negative super-saturation:



$S(t)$ - super-saturation
 $\epsilon(t)$ - volume fraction of solid
 $T(t) = \text{mid}(30, 0, -40 + |-80 + 8t|)$



Regularization of Nonsmooth DAEs

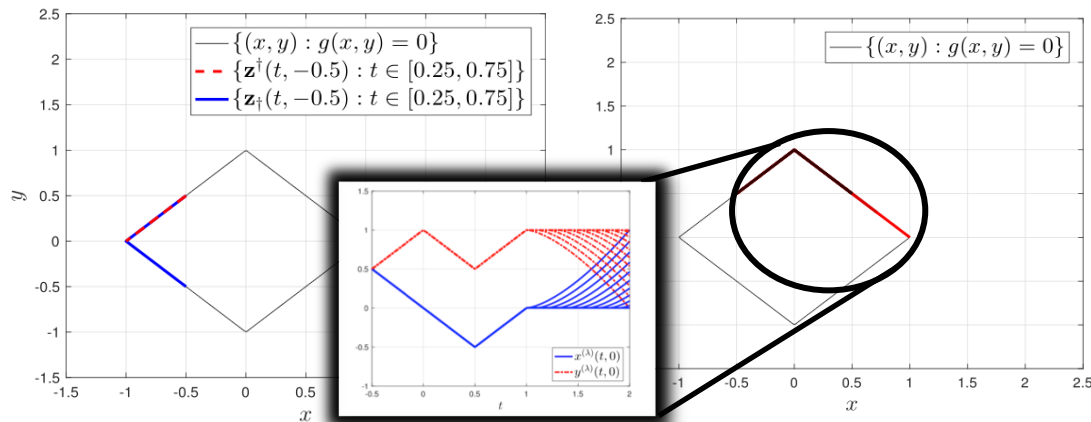
◆ Nonsmooth DAEs:

$$\dot{\mathbf{x}}(t, \mathbf{p}) = \mathbf{f}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))$$

$$\mathbf{0} = \mathbf{g}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))$$

$$\mathbf{x}(t_0, \mathbf{p}) = \mathbf{f}_0(\mathbf{p})$$

- \mathbf{f} is piecewise continuous w.r.t. t and continuous w.r.t. $\mathbf{p}, \mathbf{x}, \mathbf{y}$
- \mathbf{g} is locally Lipschitz continuous
- "Index 1" Nonsmooth DAEs: generalized differentiation index one
- Existence, uniqueness, continuous/Lipschitz dependence on parameters, etc.

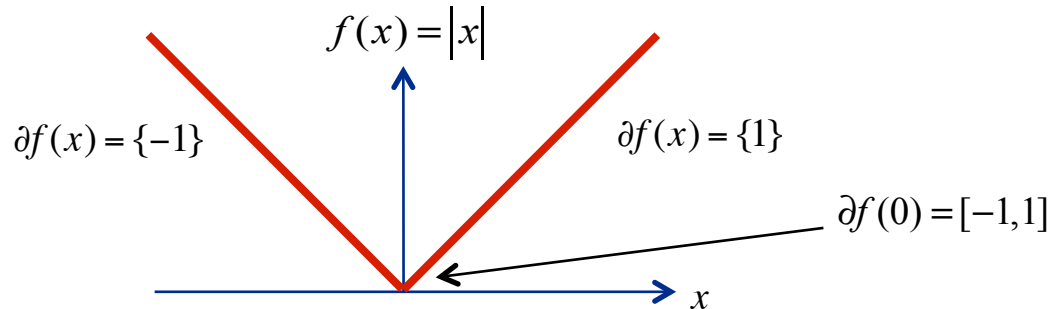


Generalized Differentiation Index

- ◆ Given locally Lipschitz continuous $\mathbf{f} : \mathbb{R}^n \rightarrow \mathbb{R}^m$:
 - Clarke's Generalized Jacobian

$$\partial \mathbf{f}(\mathbf{x}) := \text{conv} \left\{ \mathbf{H} : \mathbf{Jf}(\mathbf{x}_{(j)}) \rightarrow \mathbf{H}, \mathbf{x}_{(j)} \rightarrow \mathbf{x}, \mathbf{x}_{(j)} \in X \setminus Z_{\mathbf{f}} \right\}$$

- Example:



- "Index-1" Nonsmooth DAE:

No singular matrix in the set $\{\mathbf{M} : \exists [\mathbf{N} \ \mathbf{M}] \in \partial \mathbf{g}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))\}$

» If \mathbf{g} is C^1 : $\left\{ \begin{array}{c} \frac{\partial \mathbf{g}}{\partial \mathbf{y}}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p})) \end{array} \right\}$

MIT The "Red-line" Novartis-MIT Center

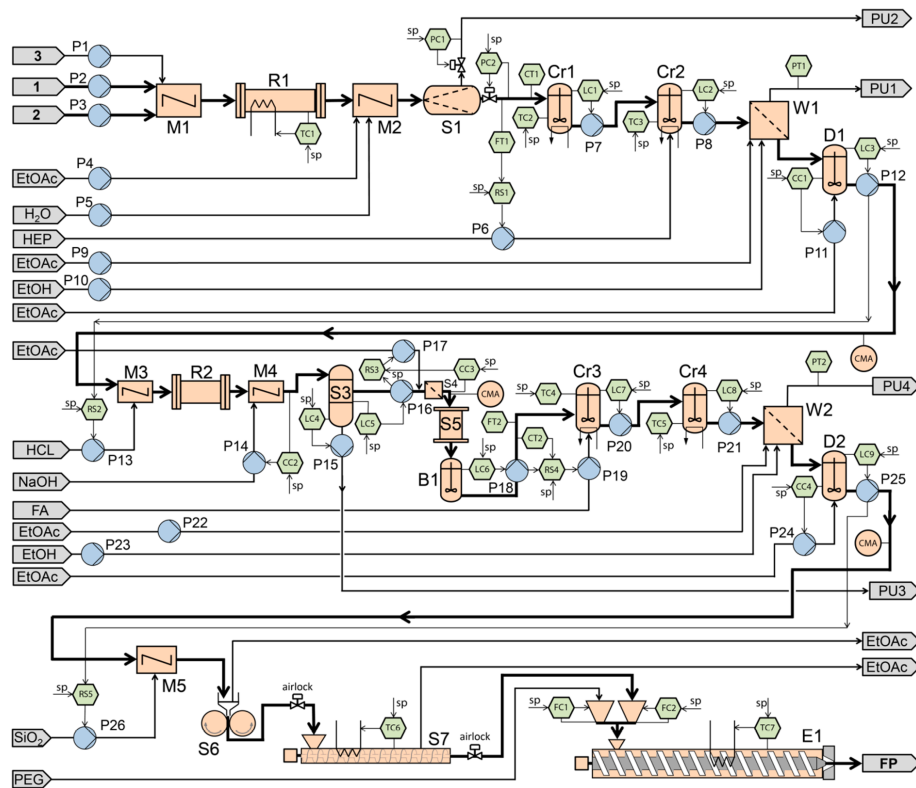


Mascia et al. "End-to-End Continuous Manufacturing of Pharmaceuticals: Integrated Synthesis, Purification, and Final Dosage Formation", *Angew. Chem. Int. Ed.* 2013, 52, 12359 -12363

Dynamic Optimization in PSE

◆ Campaign continuous manufacturing:

- Maximize production, minimize off-spec.
- “Discrete” phenomena: start-up/shut-down, phase changes, crystal growth/dissolution, etc., etc.



Dynamic Optimization of DAEs

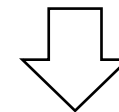
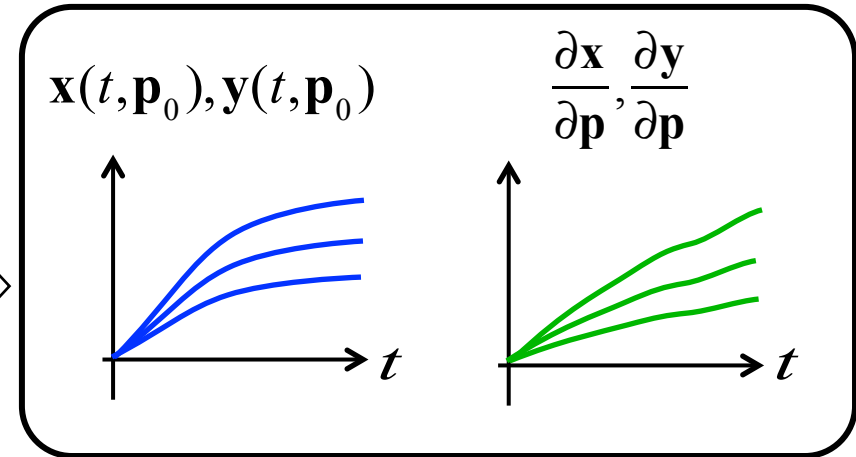
- ◆ In the smooth case:

- Semi-explicit index-1 DAE IVP

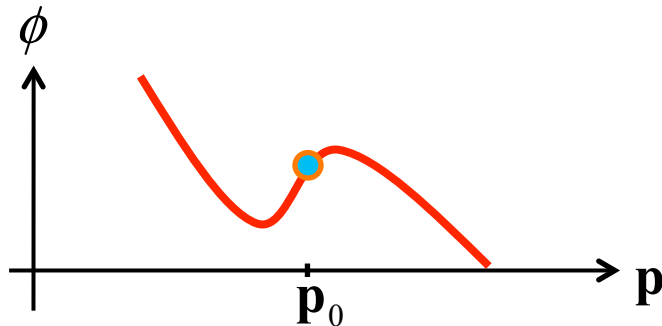
$$\begin{aligned} \dot{\mathbf{x}}(t, \mathbf{p}) &= \mathbf{f}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p})) \\ \mathbf{0} &= \mathbf{g}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p})) \\ \mathbf{x}(t_0, \mathbf{p}) &= \mathbf{f}_0(\mathbf{p}) \end{aligned}$$

- Sensitivity DAEs

$$\begin{aligned} \frac{\partial \dot{\mathbf{x}}}{\partial \mathbf{p}} &= \frac{\partial \mathbf{f}}{\partial \mathbf{p}} + \frac{\partial \mathbf{f}}{\partial \mathbf{x}} \frac{\partial \mathbf{x}}{\partial \mathbf{p}} + \frac{\partial \mathbf{f}}{\partial \mathbf{y}} \frac{\partial \mathbf{y}}{\partial \mathbf{p}} \\ \mathbf{0} &= \frac{\partial \mathbf{g}}{\partial \mathbf{p}} + \frac{\partial \mathbf{g}}{\partial \mathbf{x}} \frac{\partial \mathbf{x}}{\partial \mathbf{p}} + \frac{\partial \mathbf{g}}{\partial \mathbf{y}} \frac{\partial \mathbf{y}}{\partial \mathbf{p}} \\ \frac{\partial \mathbf{x}}{\partial \mathbf{p}}(t_0) &= \mathbf{Jf}_0(\mathbf{p}_0) \end{aligned}$$



Update \mathbf{p} via optimization



Dynamic Optimization of DAEs

- ◆ In the **nonsmooth** case:

- Semi-explicit "index-1" DAE IVP

$$\dot{\mathbf{x}}(t, \mathbf{p}) = \mathbf{f}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))$$

$$\mathbf{0} = \mathbf{g}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))$$

$$\mathbf{x}(t_0, \mathbf{p}) = \mathbf{f}_0(\mathbf{p})$$

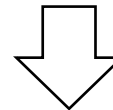
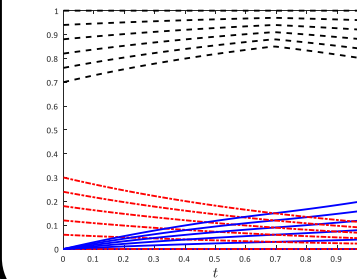
- **Nonsmooth** sensitivity DAEs

???

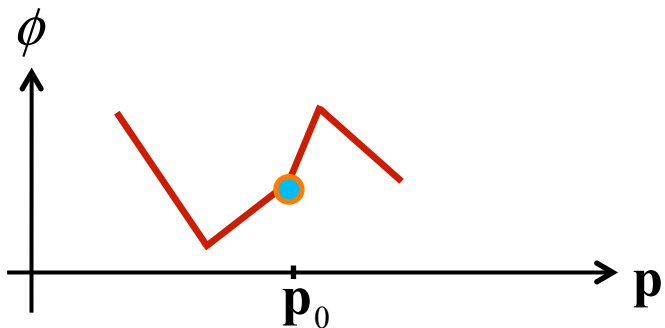
$$\mathbf{x}(t, \mathbf{p}_0), \mathbf{y}(t, \mathbf{p}_0)$$

$$\frac{\partial \mathbf{x}}{\partial \mathbf{p}}, \frac{\partial \mathbf{y}}{\partial \mathbf{p}}$$

???



Update \mathbf{p} via optimization

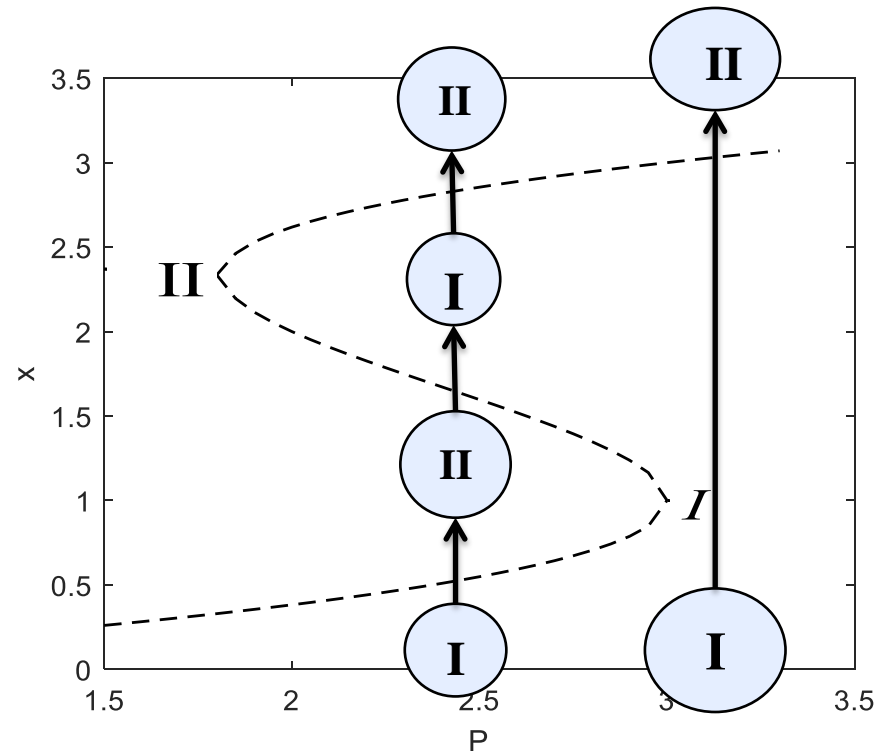
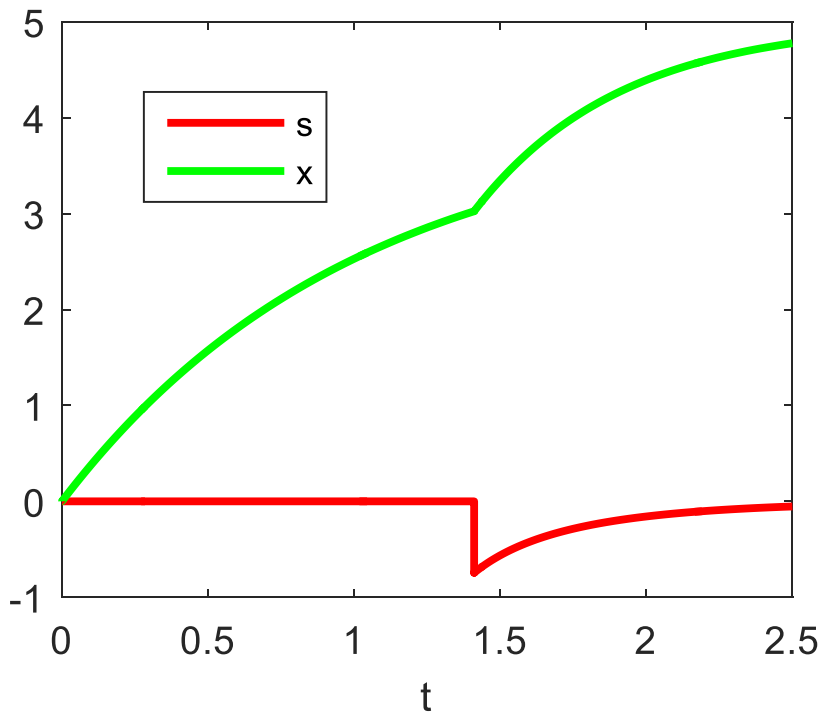


Sensitivities of Hybrid Automata

$$\dot{\mathbf{x}}^{(k)} = \mathbf{f}^{(k)}(t, \mathbf{p}, \mathbf{x}^{(k)}), \quad \mathbf{S}^{(k)} \equiv \frac{\partial \mathbf{x}^{(k)}}{\partial \mathbf{p}}$$

Transversality: $\frac{\partial g^{(k)}}{\partial \mathbf{x}^{(k)}} \dot{\mathbf{x}}^{(k)} \neq 0$

$$\mathbf{S}^{(k+1)} - \mathbf{S}^{(k)} = - \left[\mathbf{f}^{(k+1)} - \mathbf{f}^{(k)} \right] \frac{\partial t}{\partial \mathbf{p}}$$



Nonsmooth DAE Sensitivities: Generalized Derivatives

- ◆ Want generalized derivative elements

$$\partial \mathbf{x}_{t_f}(\mathbf{p}_0), \partial \mathbf{y}_{t_f}(\mathbf{p}_0)$$

- Nonsmooth analog of $\frac{\partial \mathbf{x}}{\partial \mathbf{p}}(t_f, \mathbf{p}_0), \frac{\partial \mathbf{y}}{\partial \mathbf{p}}(t_f, \mathbf{p}_0)$
- Difficult to evaluate in general (lack of sharp calculus rules, etc.)
- ◆ New tool: **lexicographic directional (LD-)derivatives**
 - Nonsmooth analog to classical directional derivative
 - Applicable to a wide class of functions (C^1 , PC^1 , convex, arbitrary compositions of such, etc.)
 - Satisfies strict calculus rules (e.g. chain rule)
 - Accurate, automatable and computationally cheap method

Lexicographic Differentiation

- ◆ $\mathbf{f} : X \in \mathbf{R}^n \rightarrow \mathbf{R}^m$ is L-smooth at $\mathbf{x} \in X$ if it is locally Lipschitz continuous and directionally differentiable, and if, for any $\mathbf{M} := [\mathbf{m}_{(1)} \cdots \mathbf{m}_{(p)}] \in \mathbf{R}^{n \times p}$, the following functions exist:

$$\mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(0)} : \mathbf{d} \mapsto \mathbf{f}'(\mathbf{x}; \mathbf{d})$$

$$\mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(1)} : \mathbf{d} \mapsto [\mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(0)}]'(\mathbf{m}_{(1)}; \mathbf{d})$$

$$\vdots$$

$$\mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(p)} : \mathbf{d} \mapsto [\mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(p-1)}]'(\mathbf{m}_{(p)}; \mathbf{d})$$

- ◆ If the columns of \mathbf{M} span \mathbf{R}^n , then $\mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(p)}$ is linear, **L-derivative**:

$$\mathbf{J}_L \mathbf{f}(\mathbf{x}; \mathbf{M}) := \mathbf{J} \mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(p)}(\mathbf{0})$$

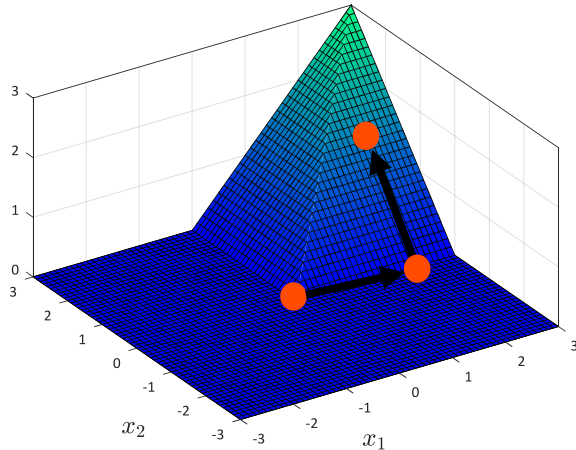
- ◆ **Lexicographic subdifferential**:

$$\partial_L \mathbf{f}(\mathbf{x}) = \{ \mathbf{J}_L \mathbf{f}(\mathbf{x}; \mathbf{M}) : \mathbf{M} \in \mathbf{R}^{n \times n}, \det \mathbf{M} \neq 0 \}$$

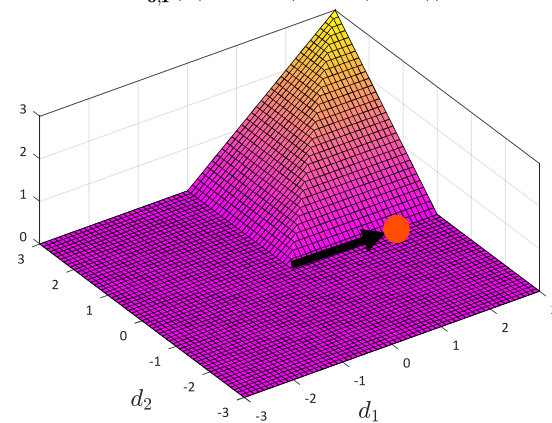
Lexicographic Differentiation

- ◆ Systematically probes local derivative information

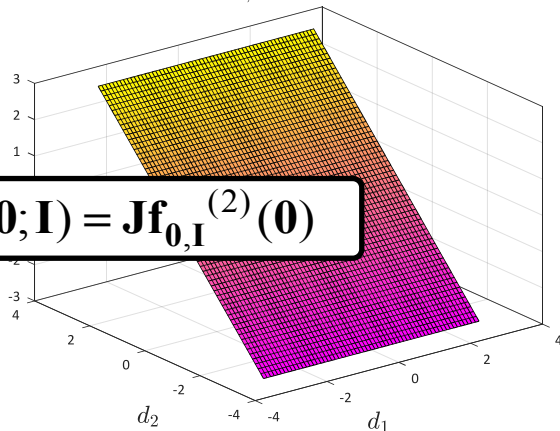
$$f(x_1, x_2) = \max(0, \min(x_1, x_2))$$



$$f_{0,\mathbf{I}}^{(0)}(\mathbf{d}) = \max(0, \min(d_1, d_2))$$

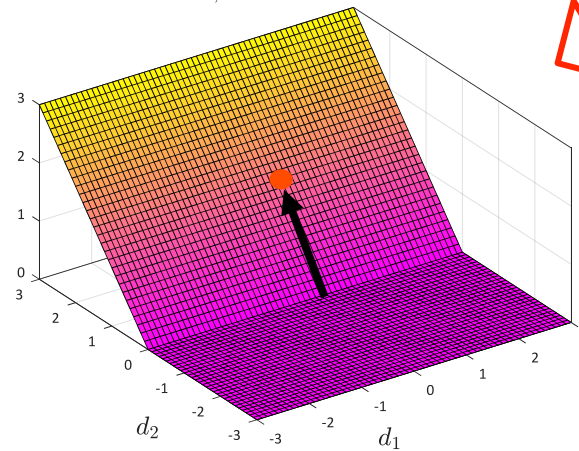


$$f_{0,\mathbf{I}}^{(2)}(\mathbf{d}) = d_2$$



$$\mathbf{J}_L \mathbf{f}(\mathbf{0}; \mathbf{I}) = \mathbf{J} \mathbf{f}_{0,\mathbf{I}}^{(2)}(\mathbf{0})$$

$$f_{0,\mathbf{I}}^{(1)}(\mathbf{d}) = \max(0, d_2)$$



LD-Derivatives

- ◆ Given L-smooth \mathbf{f} and directions matrix $\mathbf{M} := \begin{bmatrix} \mathbf{m}_{(1)} & \cdots & \mathbf{m}_{(k)} \end{bmatrix}$

$$\mathbf{f}'(\mathbf{x}; \mathbf{M}) := \begin{bmatrix} \mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(0)}(\mathbf{m}_{(1)}) & \mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(1)}(\mathbf{m}_{(2)}) & \cdots & \mathbf{f}_{\mathbf{x}, \mathbf{M}}^{(k-1)}(\mathbf{m}_{(k)}) \end{bmatrix}$$

- ◆ If \mathbf{M} is square and nonsingular:

$$\mathbf{f}'(\mathbf{x}; \mathbf{M}) = \mathbf{J}_L \mathbf{f}(\mathbf{x}; \mathbf{M}) \mathbf{M}$$

- ◆ If \mathbf{f} is C^1 at \mathbf{x} :

$$\mathbf{f}'(\mathbf{x}; \mathbf{M}) = \mathbf{J} \mathbf{f}(\mathbf{x}) \mathbf{M}$$

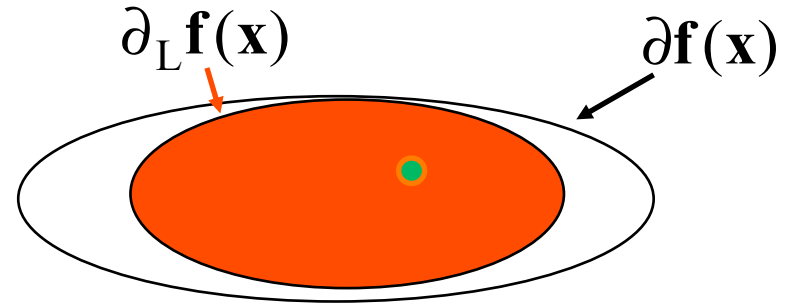
- ◆ Sharp LD-derivative chain rule:

$$\left[\mathbf{f} \circ \mathbf{g} \right]'(\mathbf{x}; \mathbf{M}) = \mathbf{f}'(\mathbf{g}(\mathbf{x}); \mathbf{g}'(\mathbf{x}; \mathbf{M}))$$

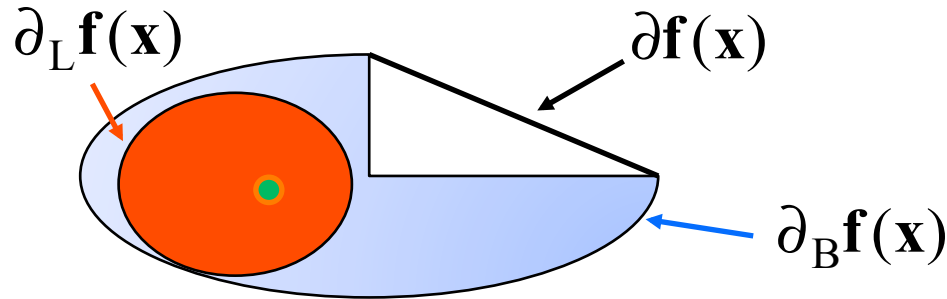
Generalized Derivatives Landscape

◆ Given $f: \mathbf{R}^n \rightarrow \mathbf{R}^m$

➤ If $m=1$ (e.g., objective function):



➤ If f is PC¹:



➤ If f is C¹:


 $\longleftarrow \partial_L \mathbf{f}(\mathbf{x}) = \partial_B \mathbf{f}(\mathbf{x}) = \partial \mathbf{f}(\mathbf{x}) = \{\mathbf{Jf}(\mathbf{x})\}$

◆ LD-derivatives furnish gen. deriv. elements (green dots) in tractable way

Dynamic Optimization of DAEs

◆ In the **nonsmooth** case:

➤ Semi-explicit "index-1" DAE IVP

$$\dot{\mathbf{x}}(t, \mathbf{p}) = \mathbf{f}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))$$

$$\mathbf{0} = \mathbf{g}(t, \mathbf{p}, \mathbf{x}(t, \mathbf{p}), \mathbf{y}(t, \mathbf{p}))$$

$$\mathbf{x}(t_0, \mathbf{p}) = \mathbf{f}_0(\mathbf{p})$$

➤ Nonsmooth sensitivities DAEs

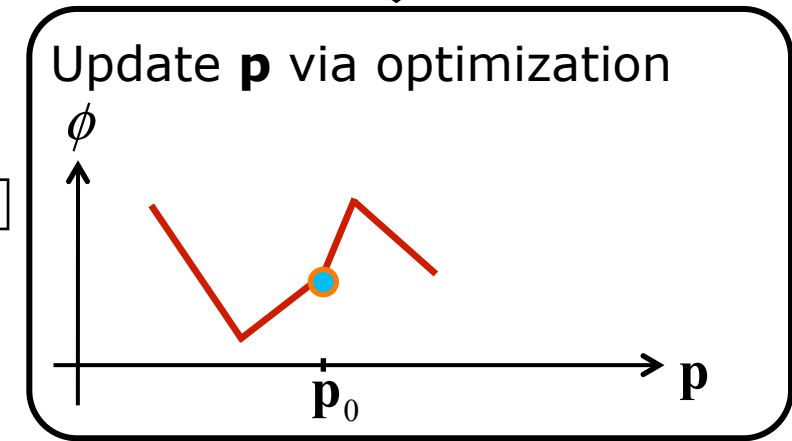
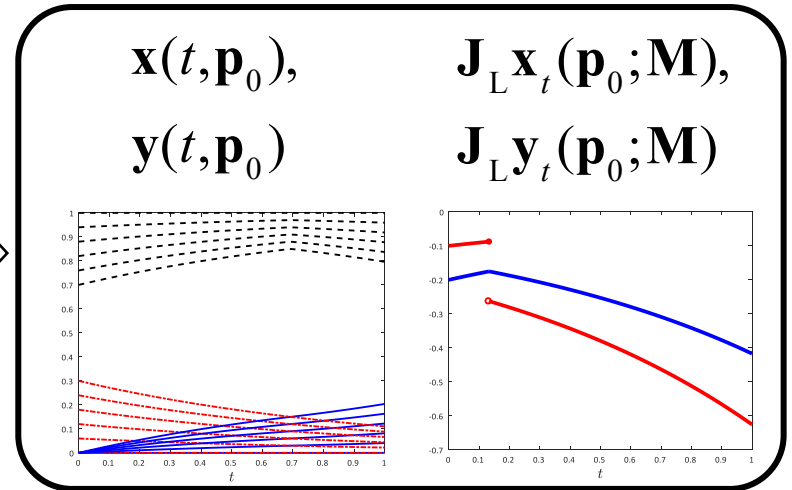
$$\dot{\mathbf{X}}(t) = [\mathbf{f}_t]'(\mathbf{p}_0, \mathbf{z}(t, \mathbf{p}_0); (\mathbf{M}, \mathbf{Z}(t)))$$

$$\mathbf{0} = [\mathbf{g}_t]'(\mathbf{p}_0, \mathbf{z}(t, \mathbf{p}_0); (\mathbf{M}, \mathbf{Z}(t)))$$

$$\mathbf{X}(t_0) = [\mathbf{f}_0]'(\mathbf{p}_0; \mathbf{M})$$

where

$$\mathbf{z} \equiv (\mathbf{x}, \mathbf{y}), \mathbf{Z} \equiv (\mathbf{X}, \mathbf{Y}) \equiv [\mathbf{z}_t]'(\mathbf{p}_0; \mathbf{M})$$



Simple Flash Process: Mode Sequence

- ◆ Mode sequence varies under parametric perturbations

$$\dot{H}(t) = U(T_{out} - T(t))$$

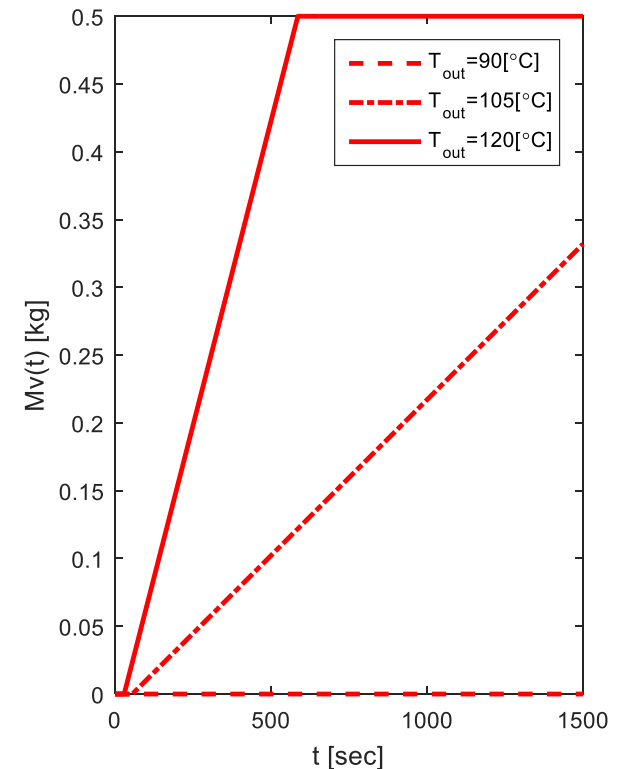
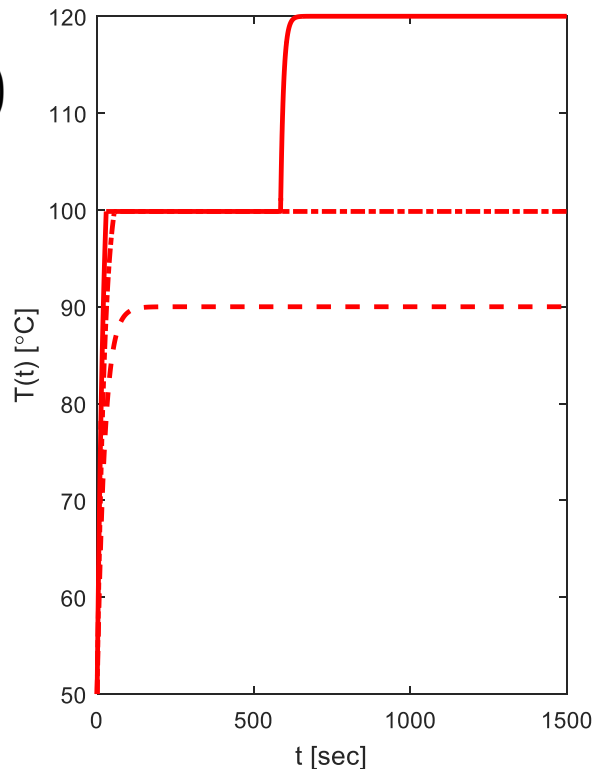
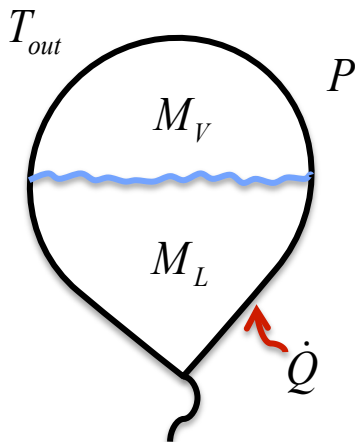
$$M = M_L(t) + M_V(t)$$

$$H(t) = Mh_v(t) - M_L(t)\Delta h_{vap}(T(t))$$

$$h_v(t) = Cp(T(t) - T_0)$$

$$\log(P^{sat}(t)) = A - B / (T(t) + C)$$

+ hybrid automaton



Simple Flash Process: Sensitivities

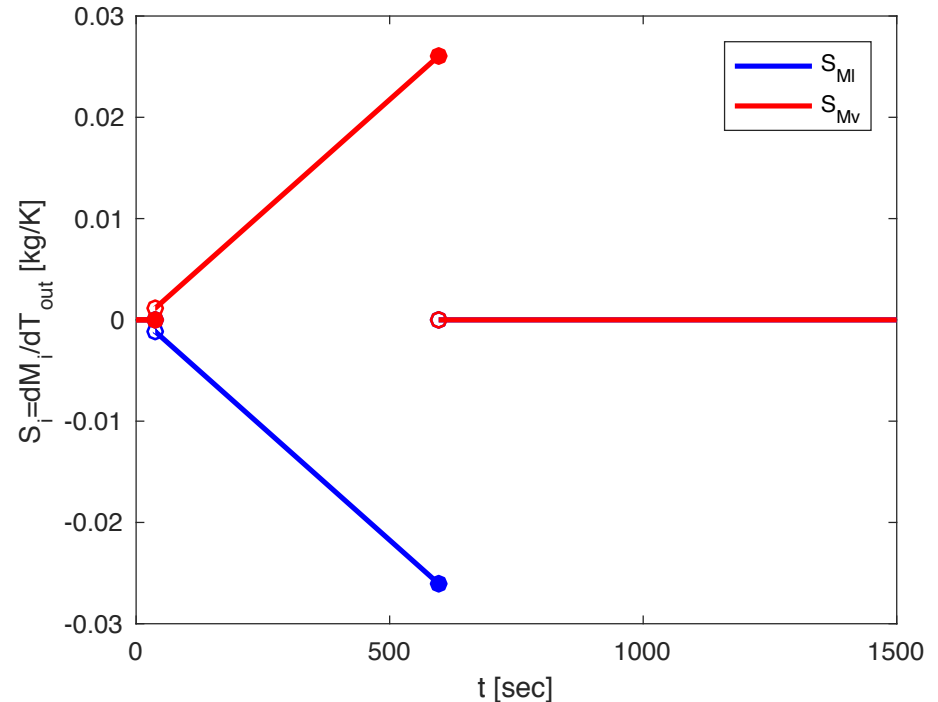
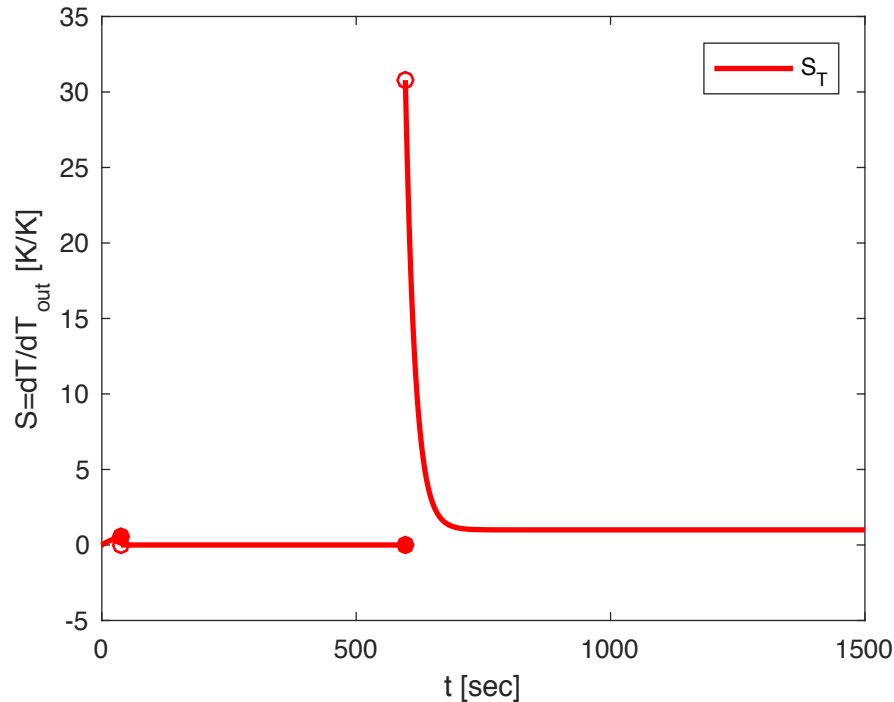
◆ Nonsmooth sensitivities:

$$\dot{S}_H(t) = U(1 - S_T(t))$$

$$S_H(t) = MCpS_T(t) - \Delta h_{vap}'(T(t))S_T(t)$$

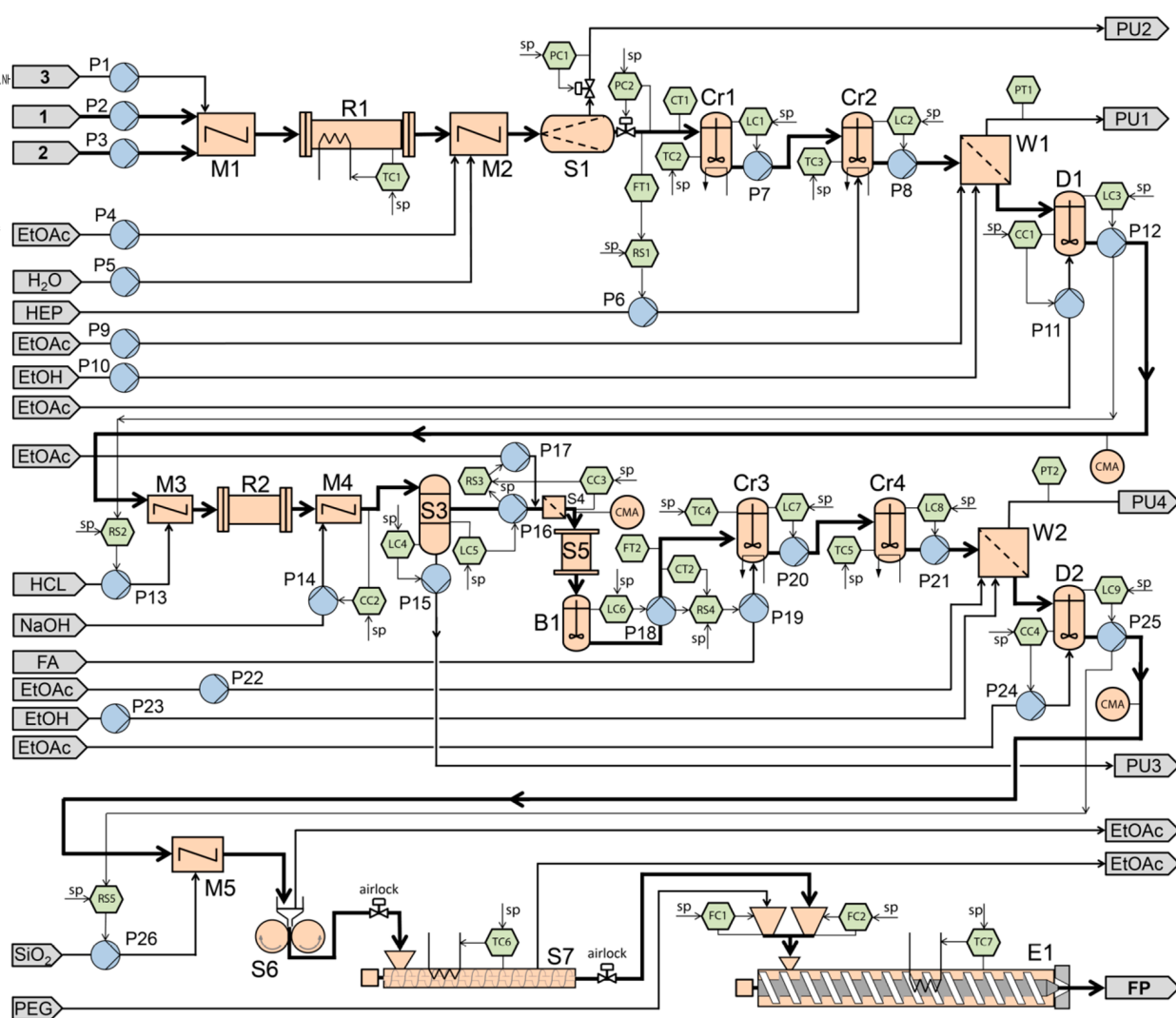
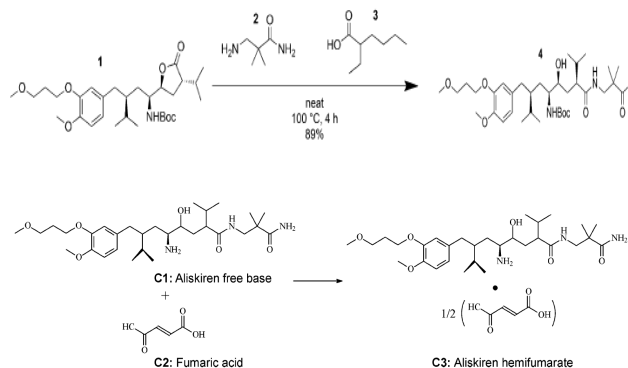
$$0 = \text{mid}'(M_V(t), P - P_{sat}(T(t)), -M_L(t); (S_V(t), -P_{sat}'(T(t))S_T(t), -S_L(t)))$$

$$S_V(t) = -S_L(t)$$



No Notion of Mode Sequence Needed

iiit The "Red-line" Process Flow Diagram



Unit operation ^[a]	t [h]
R1	4
S1	< 0.1
Cr1 + Cr2	8
W1	< 0.1
D1	2
R2	< 0.1
S3	2
S5	15
Cr3 + Cr4	8
W2	< 0.1
D2	2
S6 + S7	6
E1	< 0.1
MD	< 0.1
Total	47

Nonsmooth Process Model

No hold-up Liquid-Liquid-Equilibrium:

$$mid \left(\frac{F^{raf}}{F^{raf} + F^{pur}} - 1, \sum_{i=1}^{nc} w_i^{pur1} - \sum_{i=1}^{nc} w_i^{raf1}, \frac{F^{raf1}}{F^{raf1} + F^{pur1}} \right) = 0$$

Crystallization kinetics:

$$G(t) = \max \left(0, k_G S(t) |S(t)|^{n_G-1} \right)$$

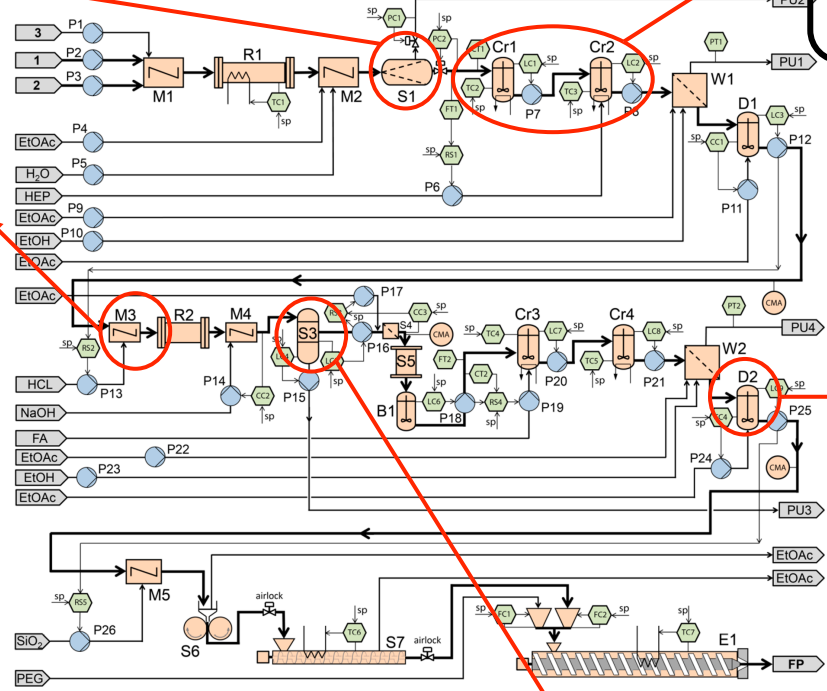
$$D(t) = \min \left(k_D S(t) |S(t)|^{n_D-1}, 0 \right)$$

Flow set point for dilution:

$$F_{S_1} = \max \left(\frac{F^{raf} w_C^{raf}}{w^{s.p}} - F^{raf}, 0 \right)$$

Valves (weirs):

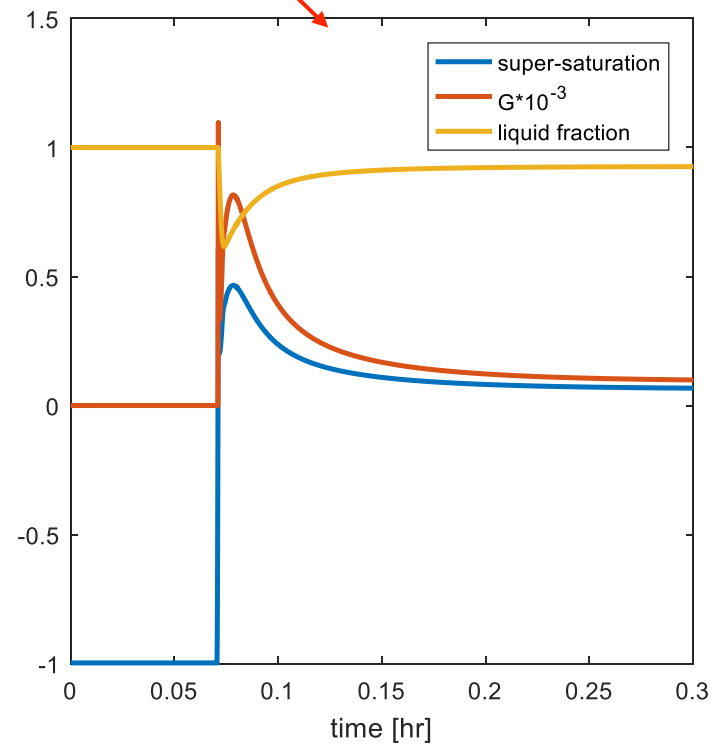
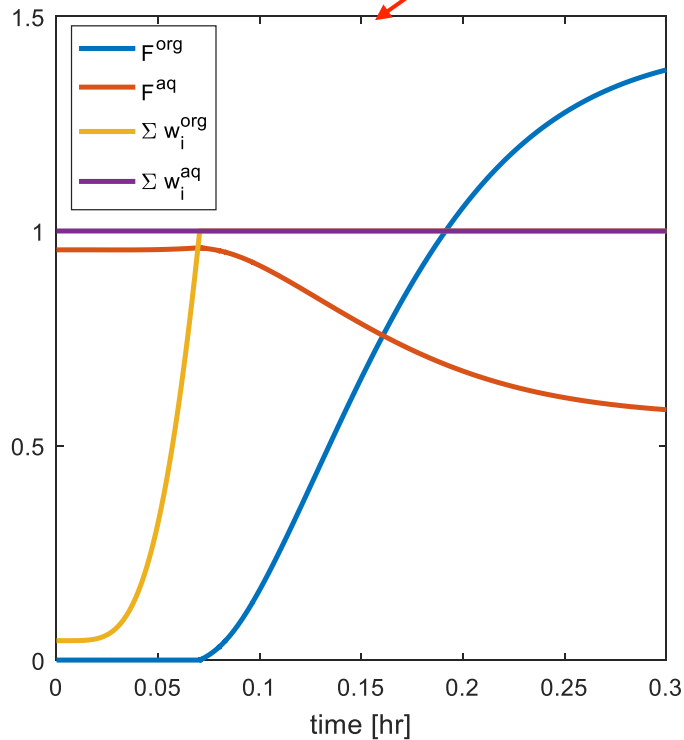
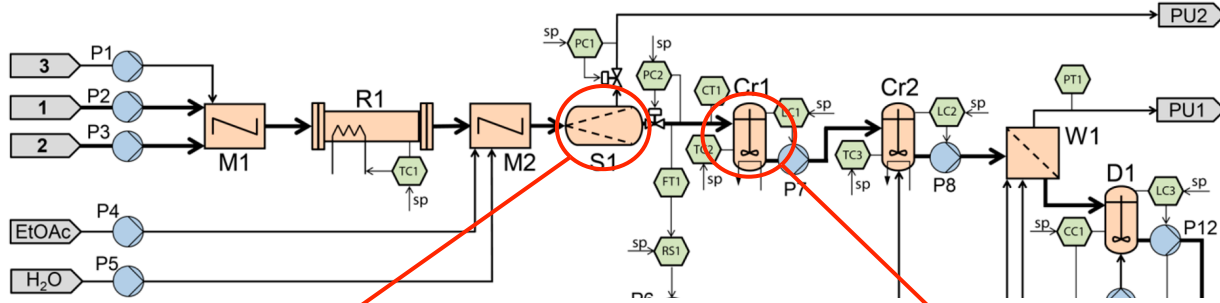
$$F_{out} = \max \left(0, u(t) \frac{V^{Cr1} - V_{min}}{\sqrt{|V^{Cr1} - V_{min}| + \epsilon}} \right)$$



Dynamic Liquid-Liquid-Equilibrium with hold-ups:

$$mid \left(\frac{M^{raf}}{M^{raf} + M^{pur}} - 1, \sum_{i=1}^{nc} w_i^{pur} - \sum_{i=1}^{nc} w_i^{raf}, \frac{M^{raf}}{M^{raf2} + M^{pur3}} \right) = 0$$

Nonsmooth Process Simulation



Dynamic Optimization: Problem formulation

Our approach, inspired by the 'turnpike theory':

$$\max_{u, t^{on}, t^{off}} \int_{t^{on}}^{t^{off}} J = \text{objective function}$$

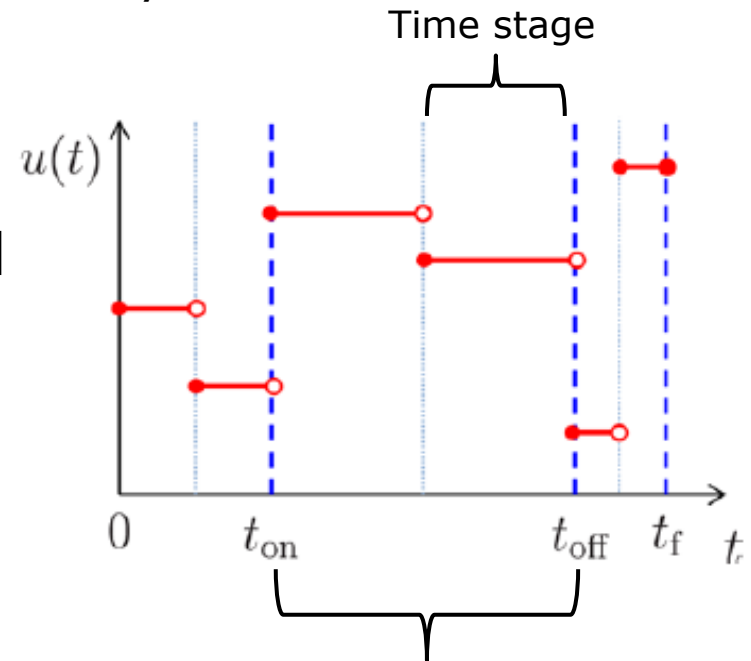
$$s.t. \quad \dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{y}, \mathbf{u}, t), \quad \mathbf{x}(0) = \mathbf{x}_0, \quad t \in [0, t^{final}]$$

$$\mathbf{0} = \mathbf{g}(\mathbf{x}, \mathbf{y}, \mathbf{u}, t)$$

safety constraints $t \in [0, t^{final}]$

quality constraints $t \in [t^{on}, t^{off}]$

final time constraints $t = t^{final}$



On-spec production
(where quality constraints are met)

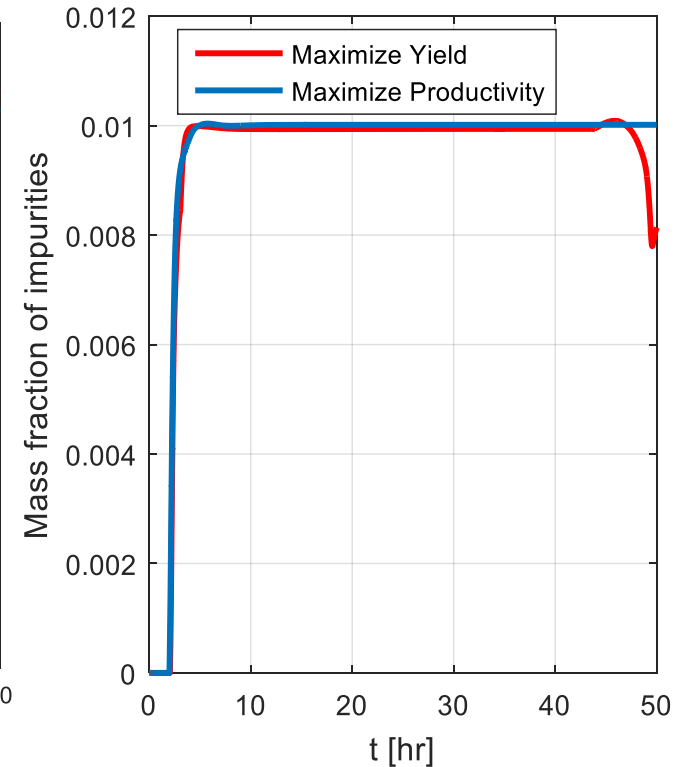
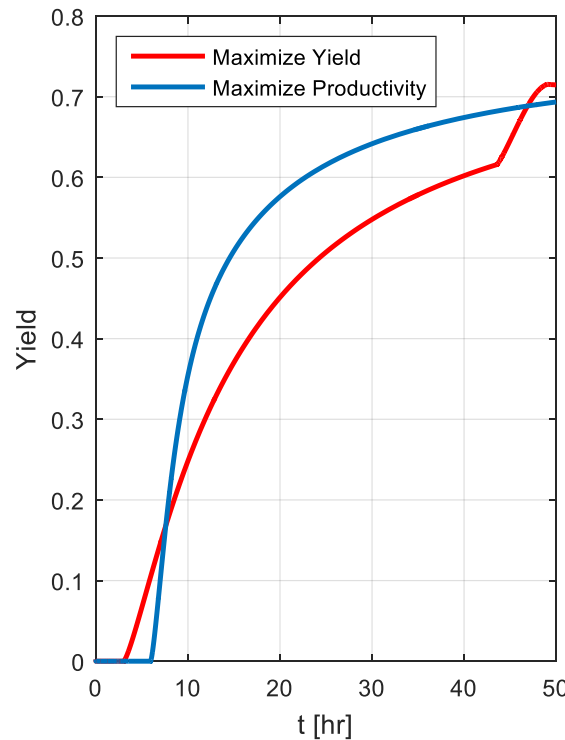
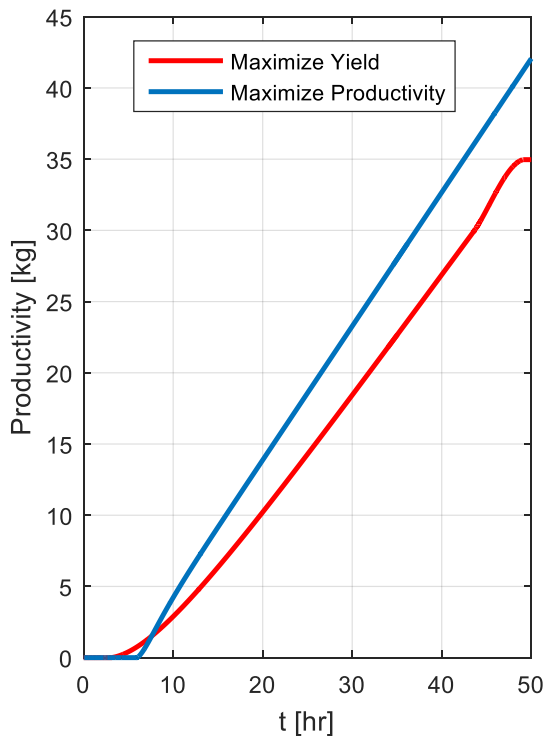
Comparison to the classical approach:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{y}, \mathbf{u}, t) = \mathbf{0}, \quad \forall t \in [t^{on}, t^{off}]$$

Case study: Multi Objective Optimization

$$\max \text{ Yield} = \frac{MW^{C1}}{MW^P} \int_{t_{on}}^{t_{off}} F_{on-spec}^P \Big/ \int_0^{t_f} F_{C1}$$

$$\max \text{ Productivity} = \int_{t_{on}}^{t_{off}} F_{on-spec}^P$$



Case study: Pareto Curves

max $Yield$

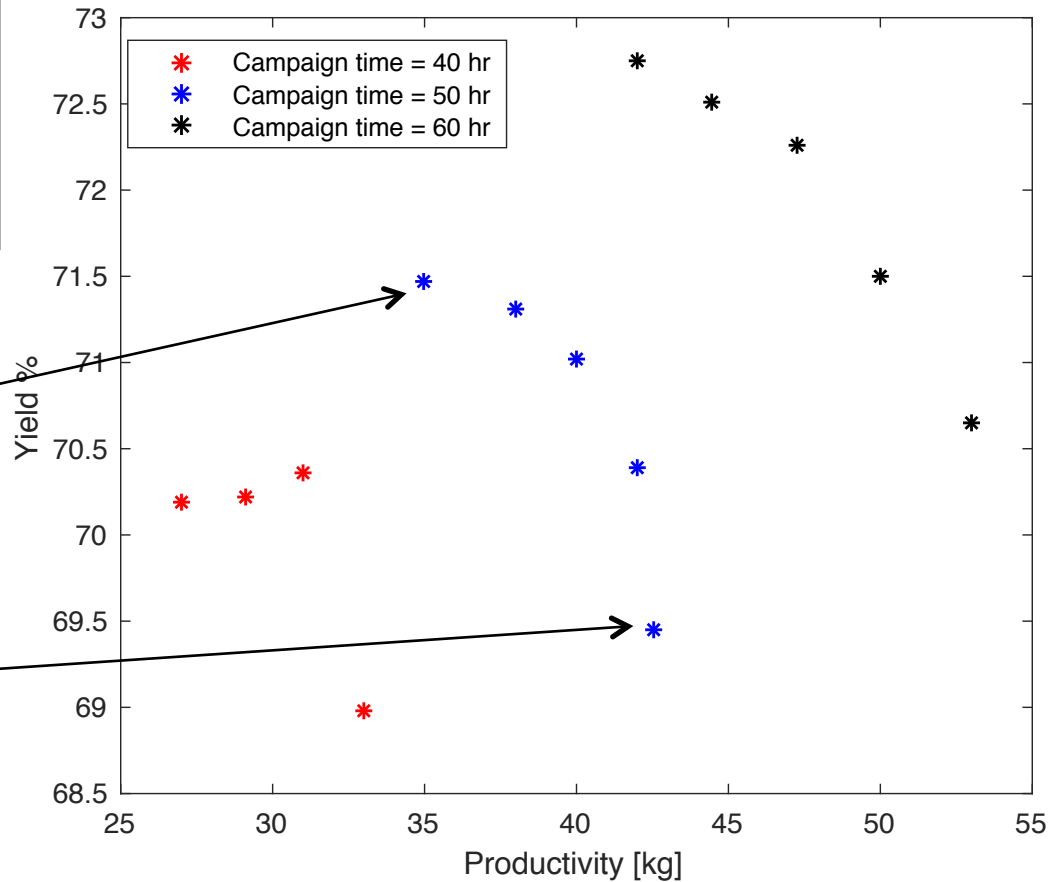
s.t

$$\left. \begin{array}{l} x_p > 0.26 \\ \sum x_I < 0.01 \end{array} \right\} \text{quality constraints}$$

$$\int_{t_{on}}^{t_{off}} F_{on-spec}^P = M^P \quad \text{operational constraint}$$

Maximize yield

Maximize productivity



Nonsmooth DAEs

◆ Summary of Progress:

- Possess a strong mathematical theory (recently)
 - » Hence, **formulate model this way if you can!**
- Easy-to-use and solve and do sensitivity analysis
- Applicable to variety of operational problems:
 - » See Sahlodin, Watson and Barton, *AIChE Journal* 62 (2016)
- Numerical toolkit: amenable to computationally tractable (e.g. automatic differentiation) methods
 - » See Khan and Barton, *OM&S* 30 (2015)
 - » LD-derivative rules for abs, min, max, mid, 2-norm, etc.

◆ Future Work:

- Numerical implementations
- “High-index” nonsmooth DAEs
- Adjoint sensitivities

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 - Natural Sciences and Engineering Research Council of Canada (NSERC)



Flow Transitions

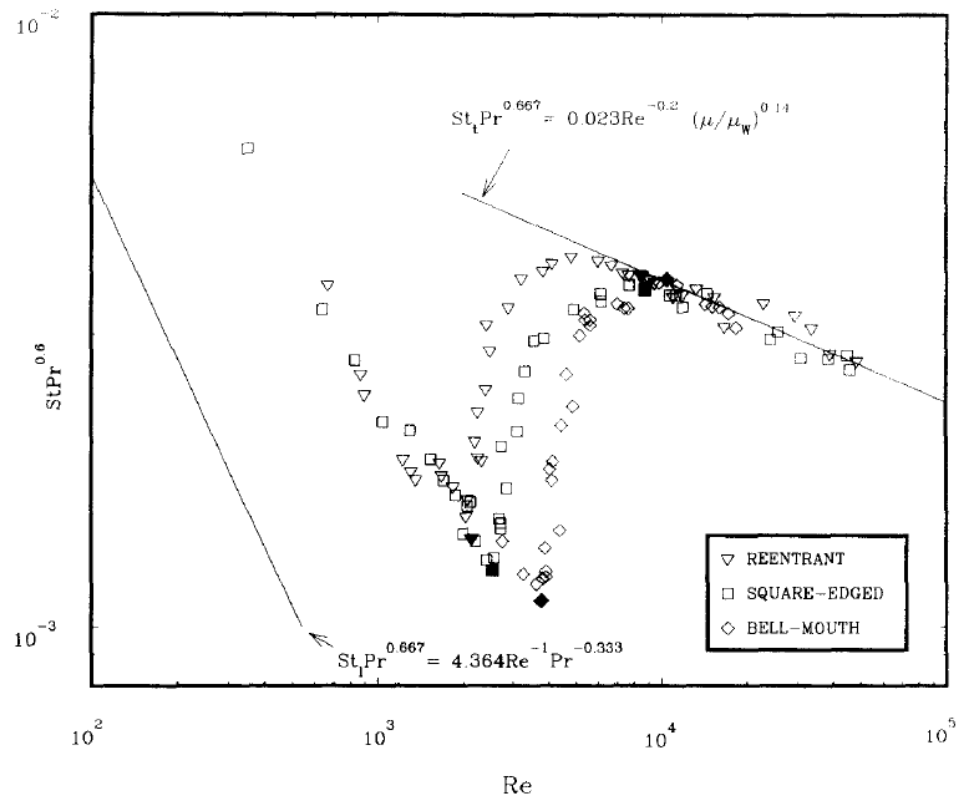
- ◆ Transitioning between flow regimes can be modeled using one nonsmooth equation

$$\text{Nu}(t) = \max(\text{Nu}_l(t), \text{Nu}_{tr}(t))$$

$$\text{Nu}_l(t) = 14.5$$

$$\text{Nu}_{tr}(t) = (\text{Nu}_l \exp((\text{Re}(t) - \text{Re}_c)/b) + \text{Nu}_t^c)^c$$

$$\text{Nu}_t(t) = 0.023 \text{Re}(t)^{0.8} \text{Pr}^{1/3}$$



Sensitivities of Nonsmooth DAEs

◆ DAE Smooth vs. Nonsmooth:

➤ Nonsmooth sensitivities:

$$\dot{\mathbf{X}}(t) = [\mathbf{f}_t]'(\mathbf{p}_0, \mathbf{x}(t, \mathbf{p}_0), \mathbf{y}(t, \mathbf{p}_0); (\mathbf{M}, \mathbf{X}(t), \mathbf{Y}(t)))$$

$$\mathbf{0} = [\mathbf{g}_t]'(\mathbf{p}_0, \mathbf{x}(t, \mathbf{p}_0), \mathbf{y}(t, \mathbf{p}_0); (\mathbf{M}, \mathbf{X}(t), \mathbf{Y}(t)))$$

$$\mathbf{X}(t_0) = [\mathbf{f}_0]'(\mathbf{p}_0; \mathbf{M})$$

- Nonsmooth and nonlinear DAE system
- Unique solution and unique initialization
- \mathbf{X} continuous, \mathbf{Y} discontinuous
- Once solved, obtain generalized derivative elements (sensitivities) via linear equation solve

➤ Smooth sensitivities:

$$\frac{\partial \dot{\mathbf{x}}}{\partial \mathbf{p}} = \frac{\partial \mathbf{f}}{\partial \mathbf{p}} + \frac{\partial \mathbf{f}}{\partial \mathbf{x}} \frac{\partial \mathbf{x}}{\partial \mathbf{p}} + \frac{\partial \mathbf{f}}{\partial \mathbf{y}} \frac{\partial \mathbf{y}}{\partial \mathbf{p}}$$

$$\mathbf{0} = \frac{\partial \mathbf{g}}{\partial \mathbf{p}} + \frac{\partial \mathbf{g}}{\partial \mathbf{x}} \frac{\partial \mathbf{x}}{\partial \mathbf{p}} + \frac{\partial \mathbf{g}}{\partial \mathbf{y}} \frac{\partial \mathbf{y}}{\partial \mathbf{p}}$$

$$\frac{\partial \mathbf{x}}{\partial \mathbf{p}}(t_0) = \mathbf{Jf}_0(\mathbf{p}_0)$$

- Linear DAE system
- Unique soln. & init.
- $\frac{\partial \mathbf{x}}{\partial \mathbf{p}}(\cdot, \mathbf{p}_0), \frac{\partial \mathbf{y}}{\partial \mathbf{p}}(\cdot, \mathbf{p}_0)$ continuous